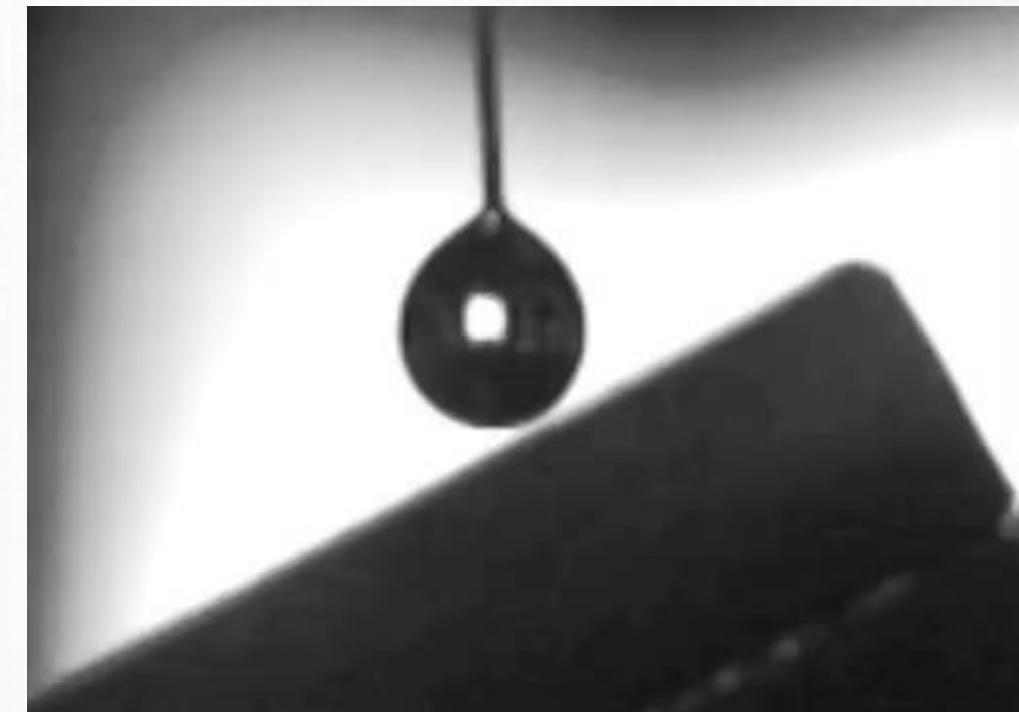




TOPOGRAPHICAL SURFACE TENSION GRADIENTS FOR EFFECTIVE WATER MANAGEMENT IN ENERGY TECHNOLOGY



Kirill Misiiuk

Sam Lowrey, Richard Blaikie,

Andrew Sommers, Geoff Willmott



ONE PLUS THREE





ONE PLUS THREE



ONE PLUS THREE

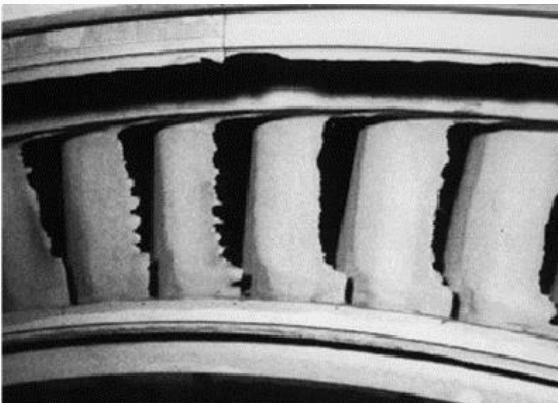


ONE PLUS THREE

Drop-impact



L. Rampel, Wind Systems Magazine (Issue date 24.10.2012) 22-24]



A. Martínez et al., J. energy power eng, 2012, 4 (5), 365-371

Condensation



David L. Chandler, MIT News Office
21 June 2013

Icing



M. Alrefai, International Conference on Renewable Energies and Power Quality, 2019



Bob Garrard, Aviation Photos
(<https://www.flickr.com/people/23032926@N05/>)

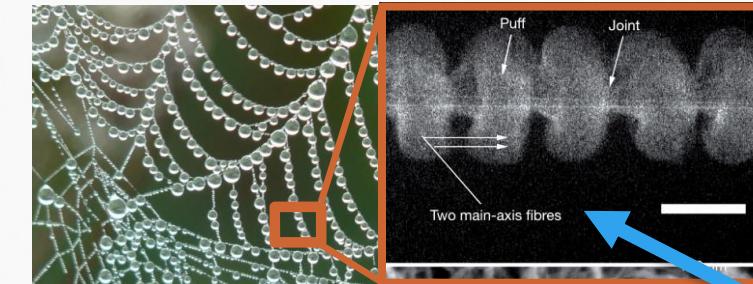
IN THE PREVIOUS EPISODE...

“Lotus effect”

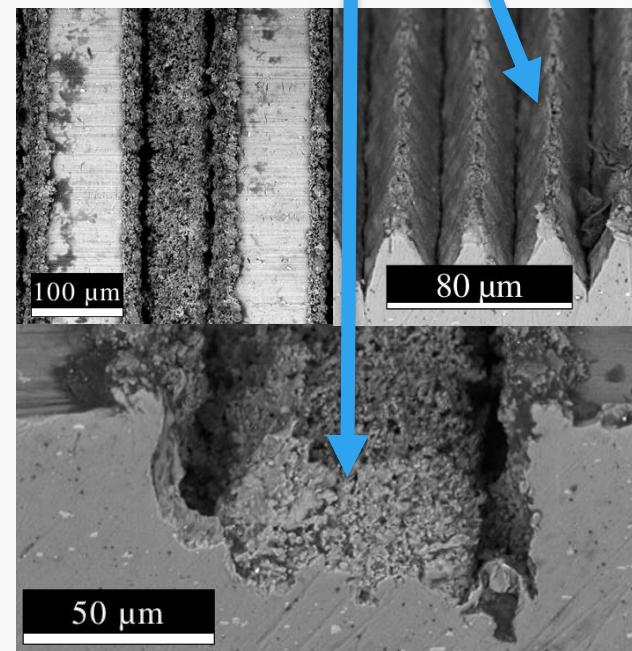
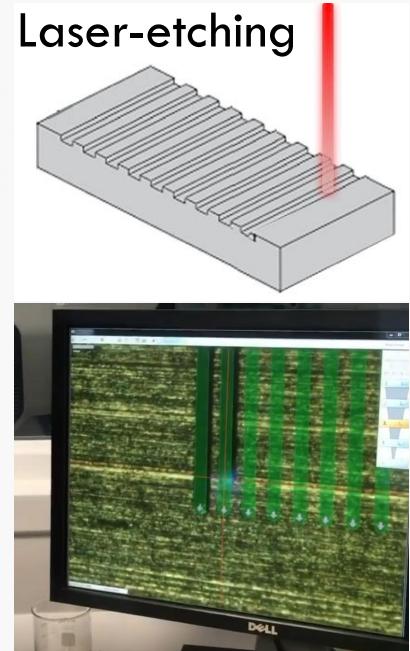


H. Zhang et al., *Colloids Surf A: Physicochem. Eng. Aspects*, 413, 2012

Spider silk

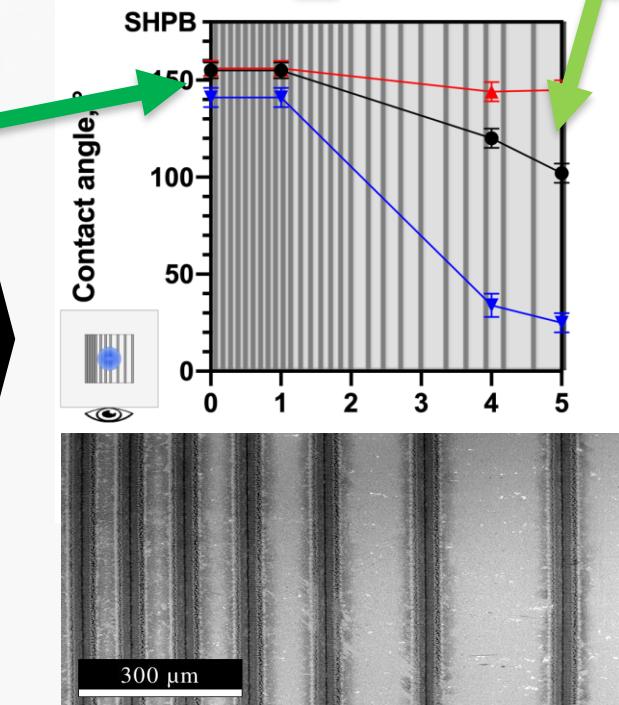
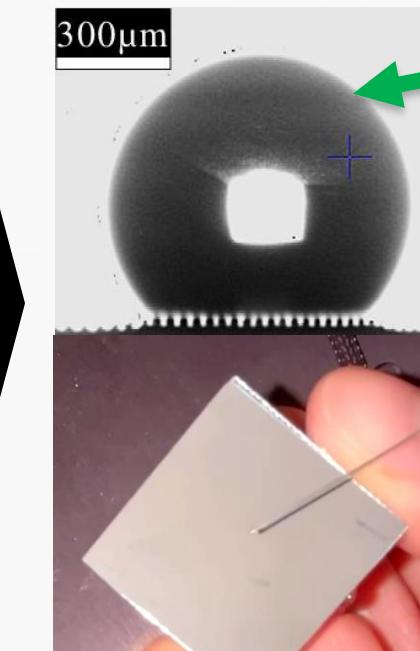


Y. Zheng et al., *Nature*, 2010



K. Misiiuk et al., *Langmuir*, 2022
DOI:10.1021/acs.langmuir.1c02517

No coatings!



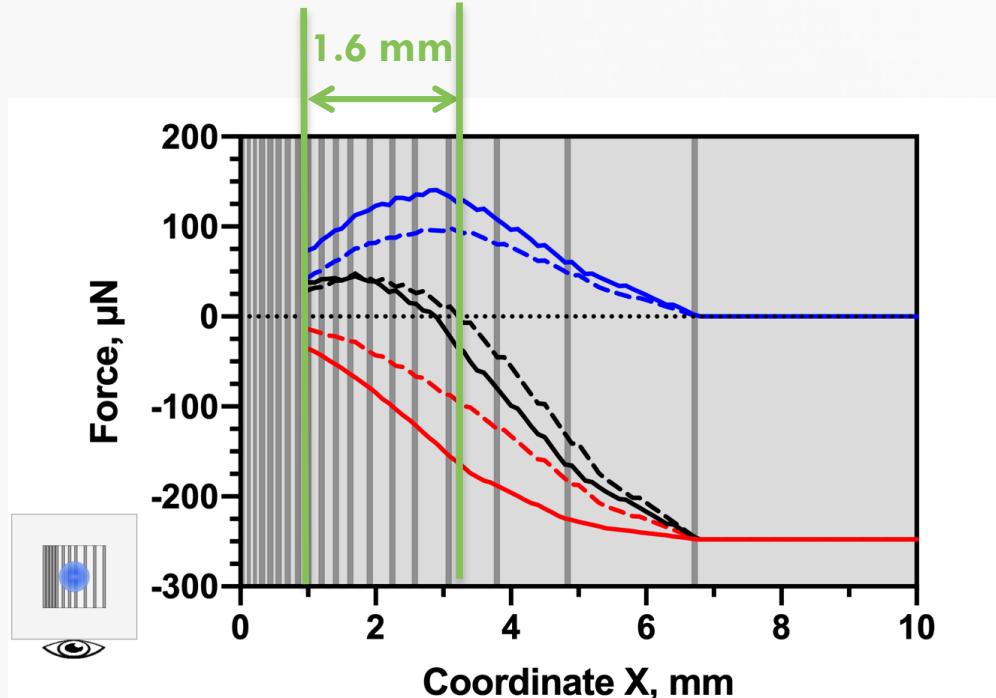
K. Misiiuk et al., *Langmuir*, 2022
DOI:10.1021/acs.langmuir.1c02518

IN THE PREVIOUS EPISODE...

$$F_{\text{acting}} = F_{\text{driving}} + F_{\text{hysteresis}} = 0$$

↓

$$\frac{df}{dx} = \frac{8f_0(\cos \theta_1 - \cos \theta_2)}{D_{FP}[(\cos \theta_2 + 1)(4 + \pi) - (\cos \theta_1 + 1)(4 - \pi)]}$$



Classic approach

Driving force

Hysteresis force

$F_d + F_h$

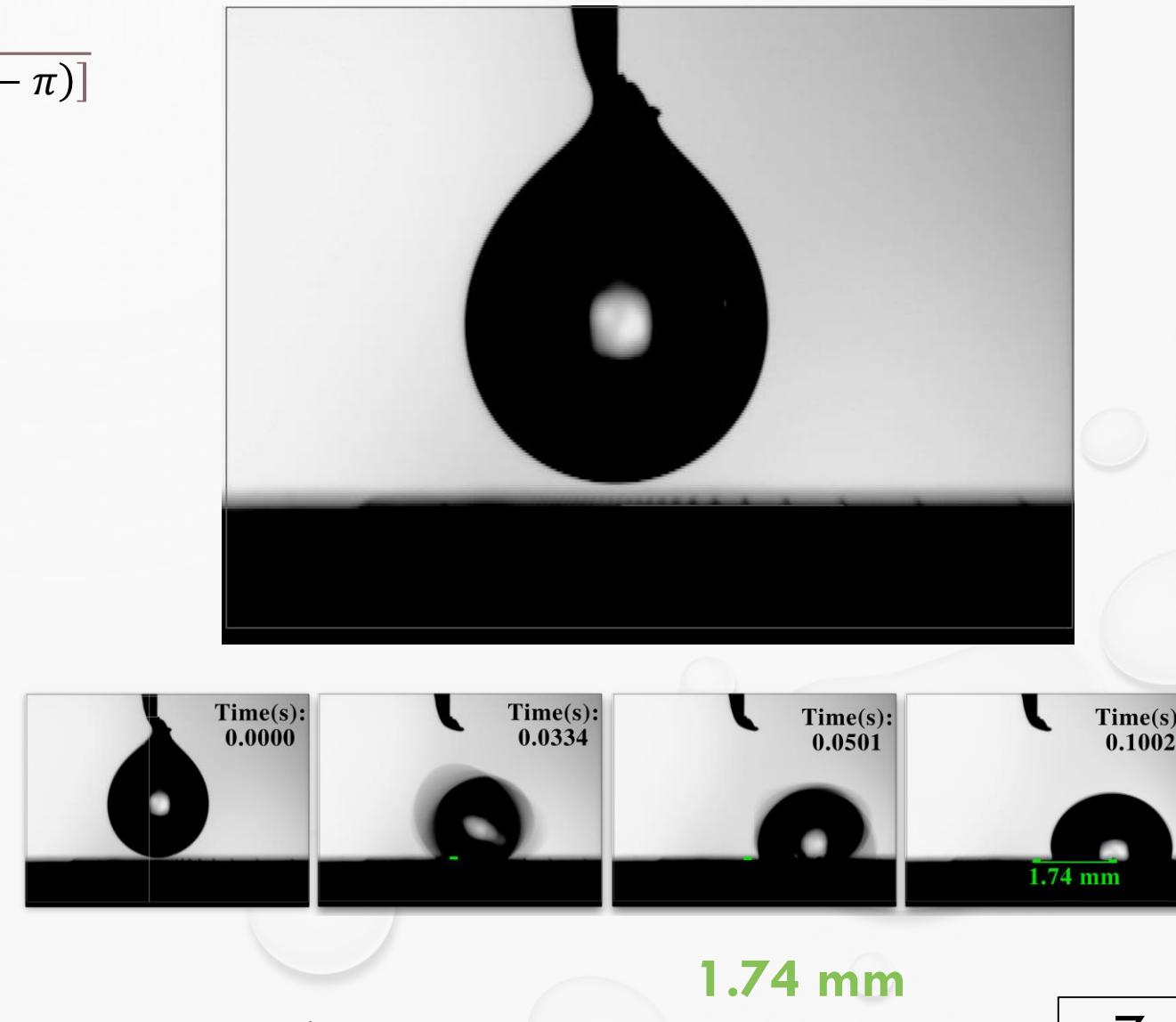
Modified approach

Driving force

Hysteresis force

$F_d + F_h$

Working principle for 8 μL droplet





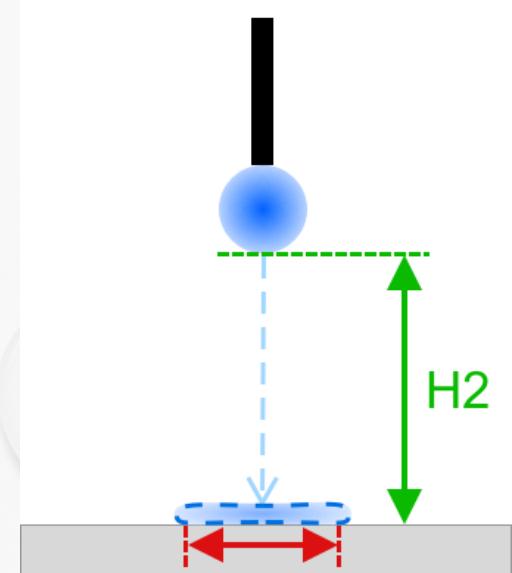
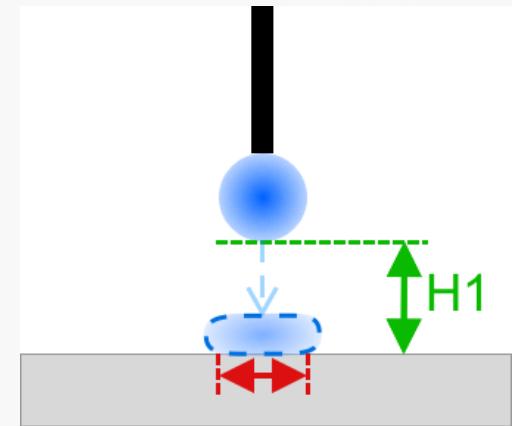
CURRENT STAGE: DROP IMPACT



University of Missouri, MUEngineering,
https://youtu.be/riXp_Q-fDv8

During impact
the **footprint** is
changing!

$$\frac{df}{dx} = \boxed{D_{FP}} \frac{8f_0(\cos \theta_1 - \cos \theta_2)}{(\cos \theta_2 + 1)(4 + \pi) - (\cos \theta_1 + 1)(4 - \pi)}$$





CURRENT STAGE: DROP IMPACT

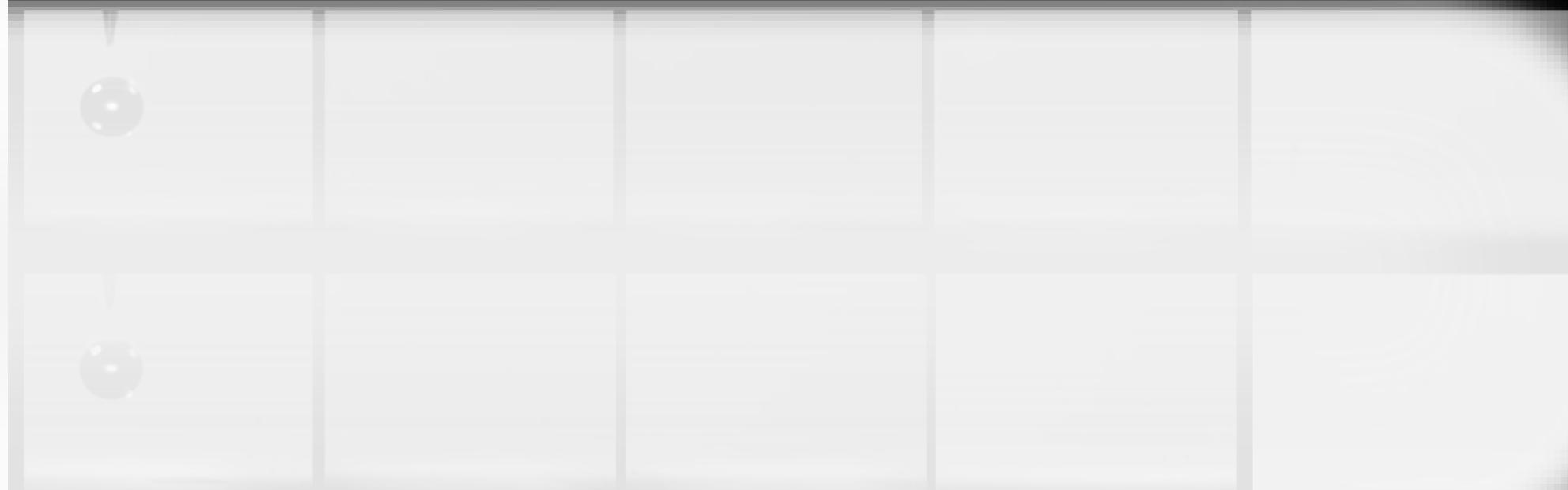
Impact velocity: 0.3 m/s



Strong gradient
($df/dx = 0.24$):

Intermediate
gradient
($df/dx = 0.11$):

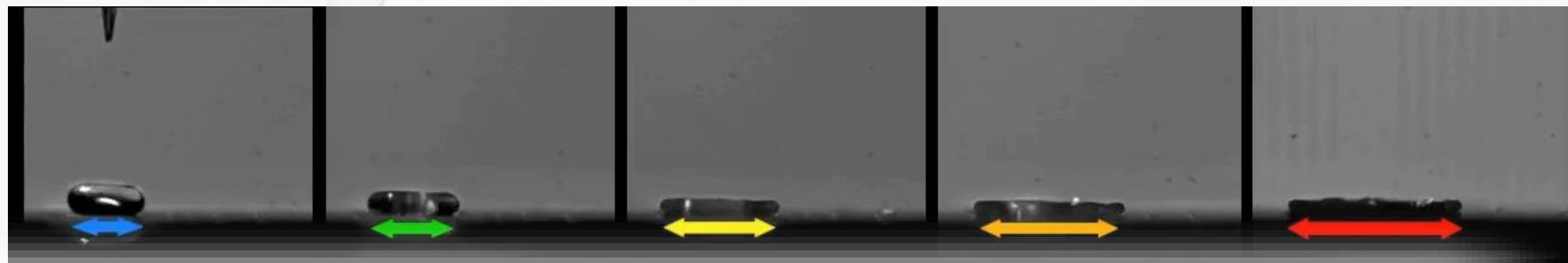
Weak gradient
(almost uniform SHPB,
 $df/dx = 0.08$):



Time: 00 ms

CURRENT STAGE: DROP IMPACT

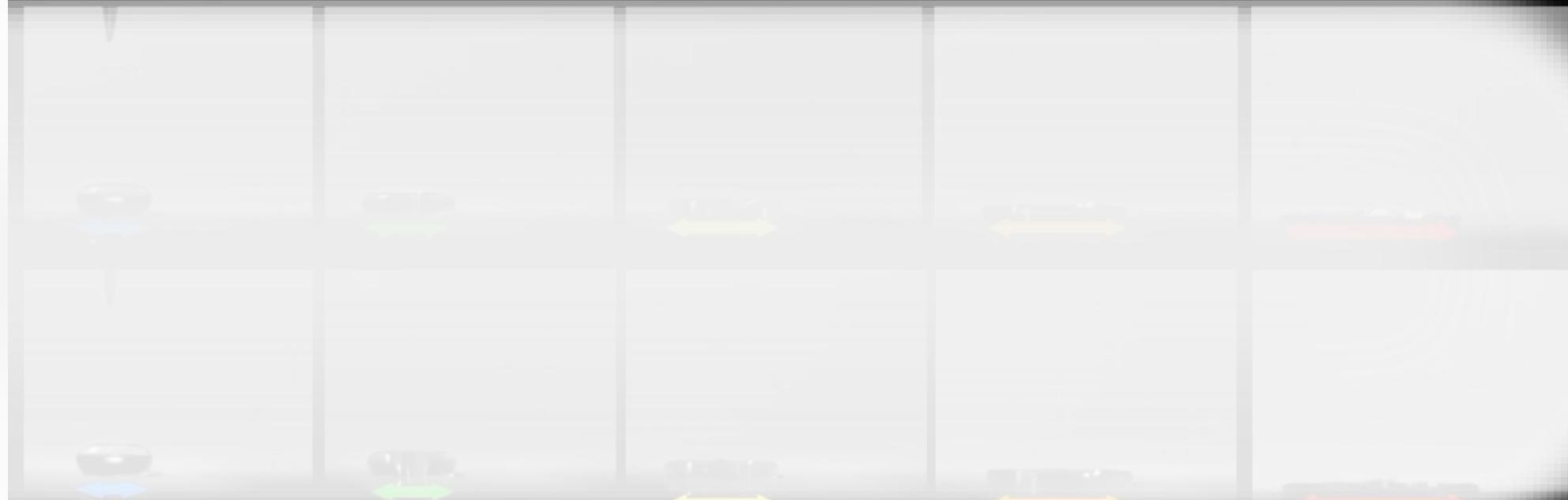
Impact velocity: 0.3 m/s



Strong gradient
($df/dx = 0.24$):

Intermediate
gradient
($df/dx = 0.11$):

Weak gradient
(almost uniform SHPB,
 $df/dx = 0.08$):

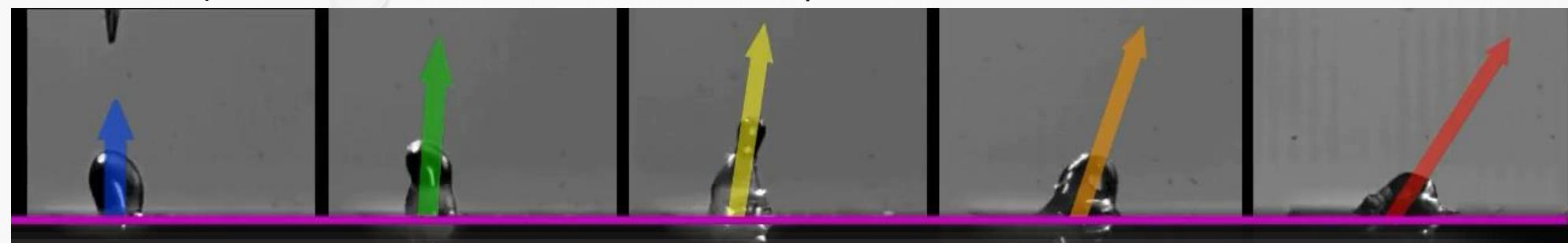


Time: 18 ms



CURRENT STAGE: DROP IMPACT

Impact velocity: 0.3 m/s



Strong gradient
($df/dx = 0.24$):



Intermediate
gradient
($df/dx = 0.11$):



Weak gradient
(almost uniform SHPB,
 $df/dx = 0.08$):

Time: 23 ms



CURRENT STAGE: DROP IMPACT

Impact velocity: 0.3 m/s



0.6 m/s

1.0 m/s

1.4 m/s

2.0 m/s

Strong gradient
($df/dx = 0.24$):



Intermediate
gradient
($df/dx = 0.11$):



Weak gradient
(almost uniform SHPB,
 $df/dx = 0.08$):

Time: 00 ms

CURRENT STAGE: DROP IMPACT

Impact velocity: 0.3 m/s

0.6 m/s

1.0 m/s

1.4 m/s

2.0 m/s

Strong gradient
 $(df/dx = 0.24)$:

Intermediate
gradient
 $(df/dx = 0.11)$:

Weak gradient
(almost uniform SHPB,
 $df/dx = 0.08$):



Time: 18 ms

CURRENT STAGE: DROP IMPACT

Impact velocity: 0.3 m/s

0.6 m/s

1.0 m/s

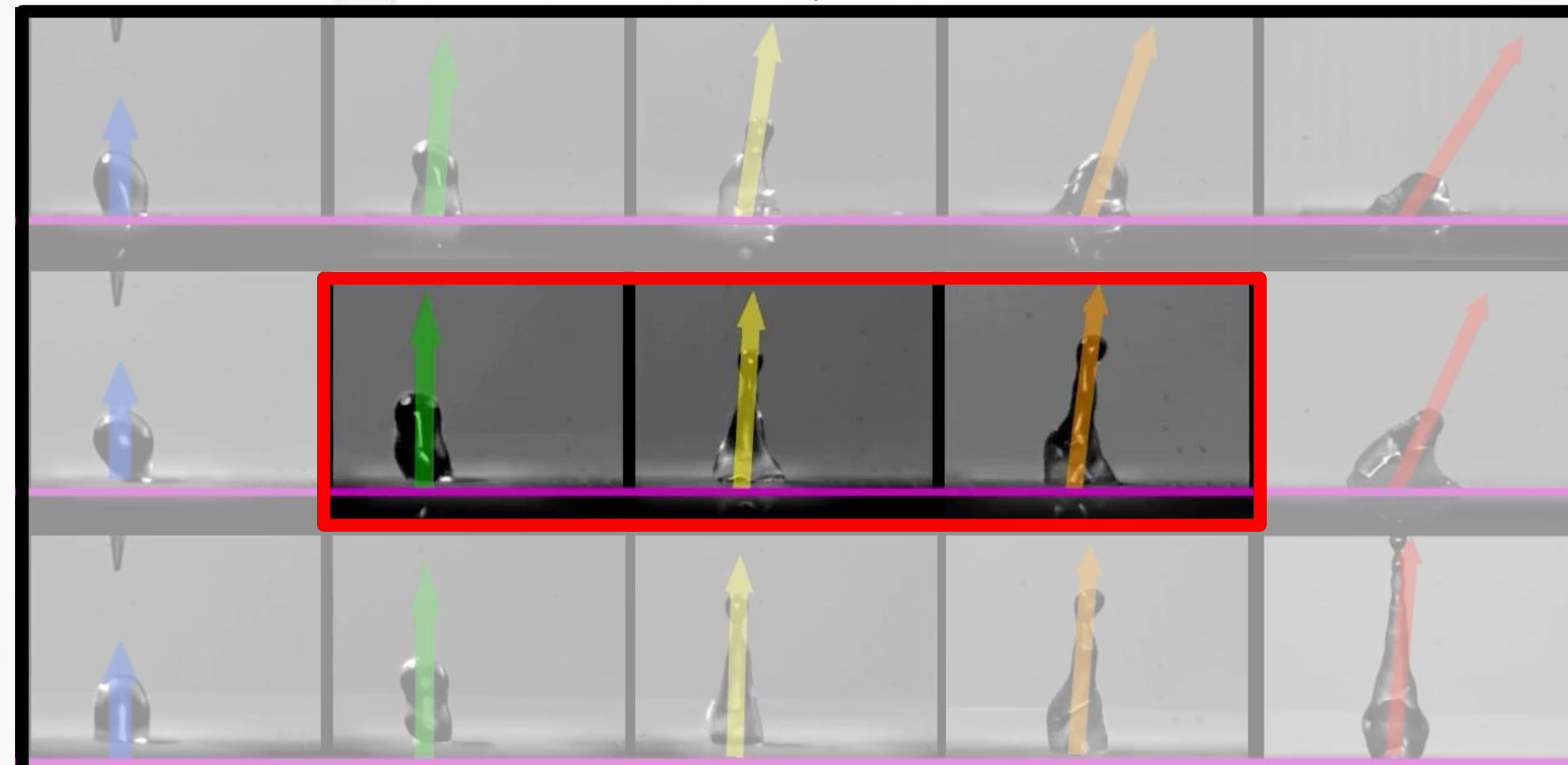
1.4 m/s

2.0 m/s

Strong gradient
 $(df/dx = 0.24)$:

Intermediate
gradient
 $(df/dx = 0.11)$:

Weak gradient
(almost uniform SHPB,
 $df/dx = 0.08$):



Time: 23 ms

CURRENT STAGE: DROP IMPACT

Impact velocity: 0.3 m/s

0.6 m/s

1.0 m/s

1.4 m/s

2.0 m/s

Strong gradient
 $(df/dx = 0.24)$:

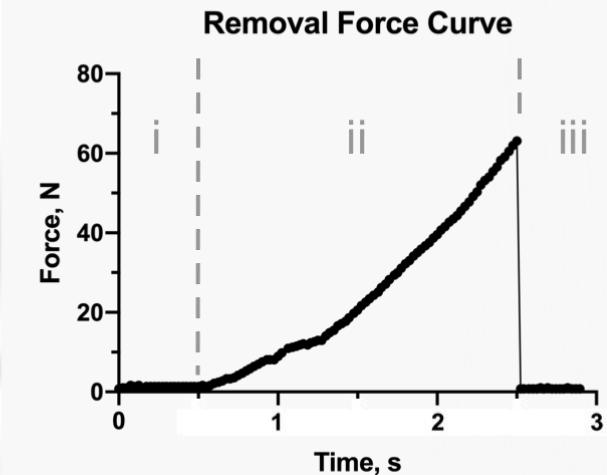
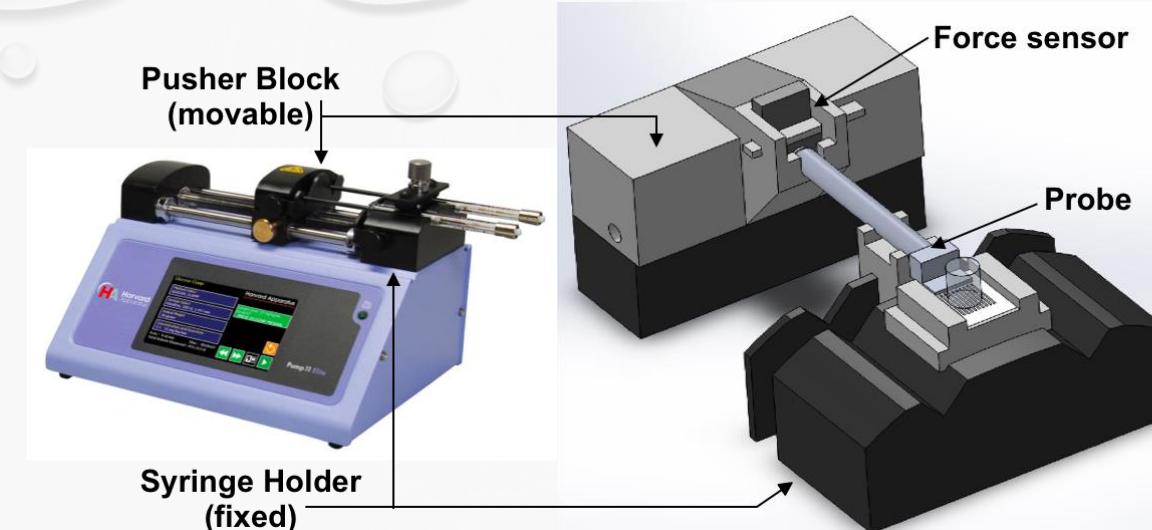
Intermediate
gradient
 $(df/dx = 0.11)$:

Weak gradient
(almost uniform SHPB,
 $df/dx = 0.08$):



Time: 23 ms

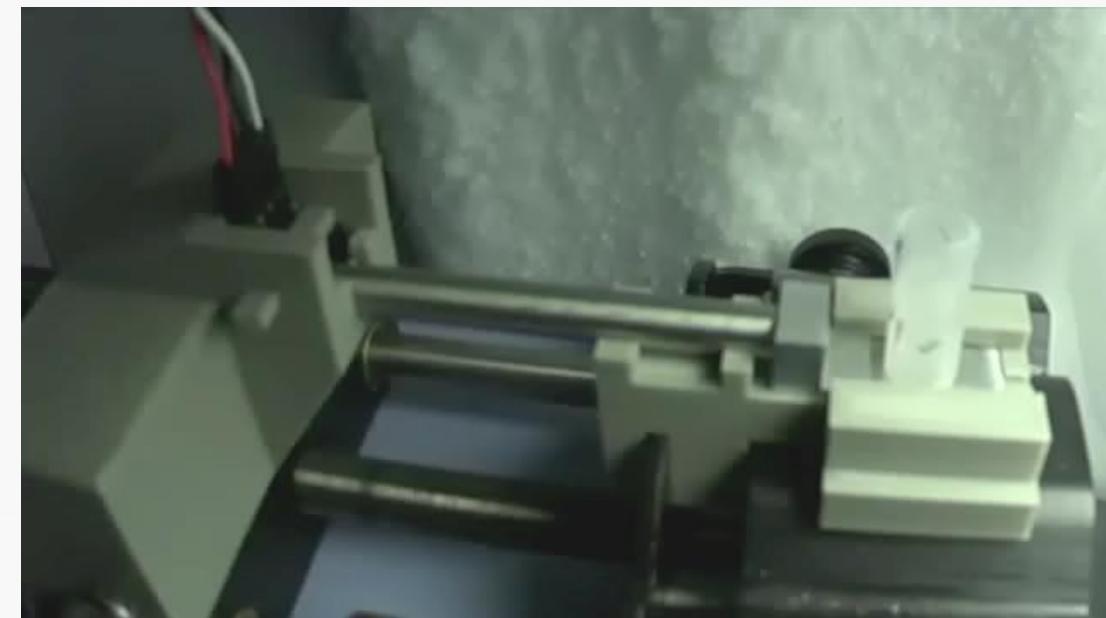
CURRENT STAGE: ICE ADHESION



The setup overview

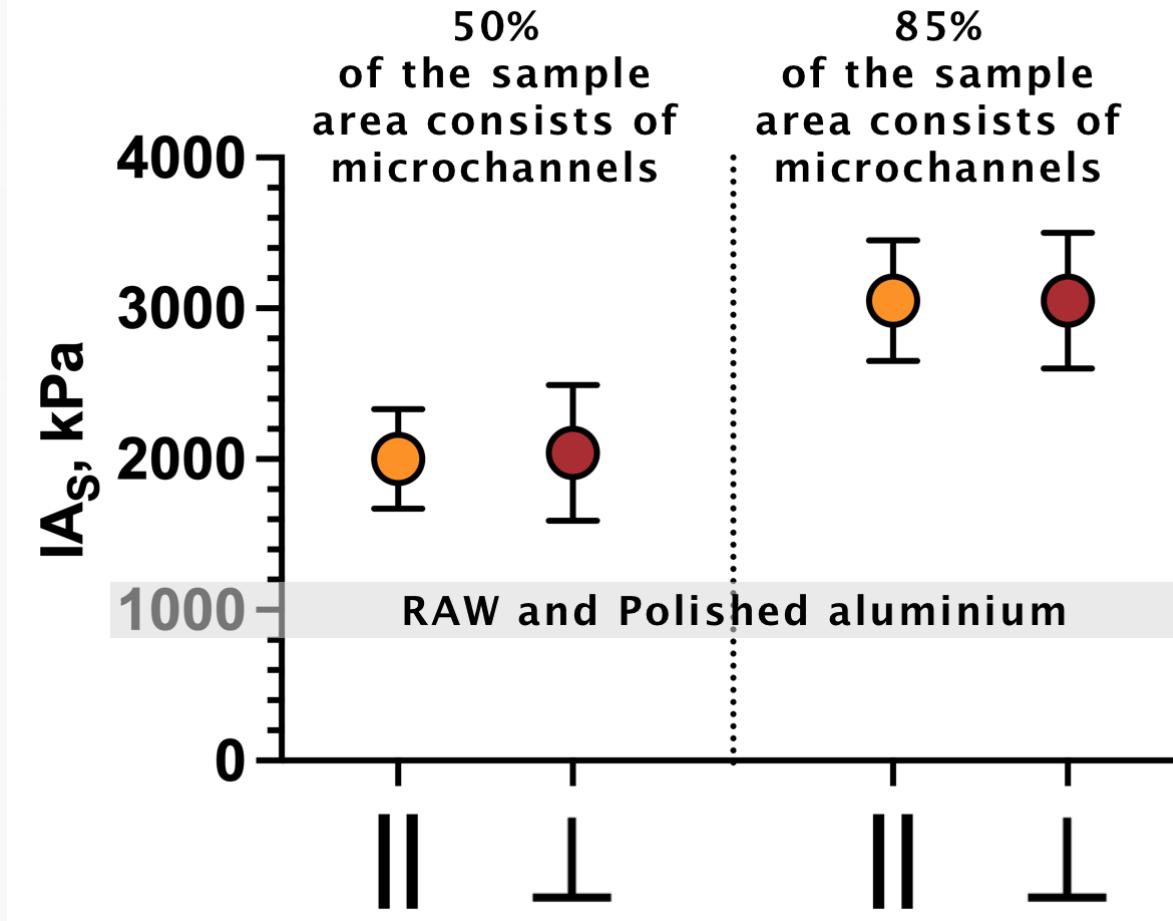
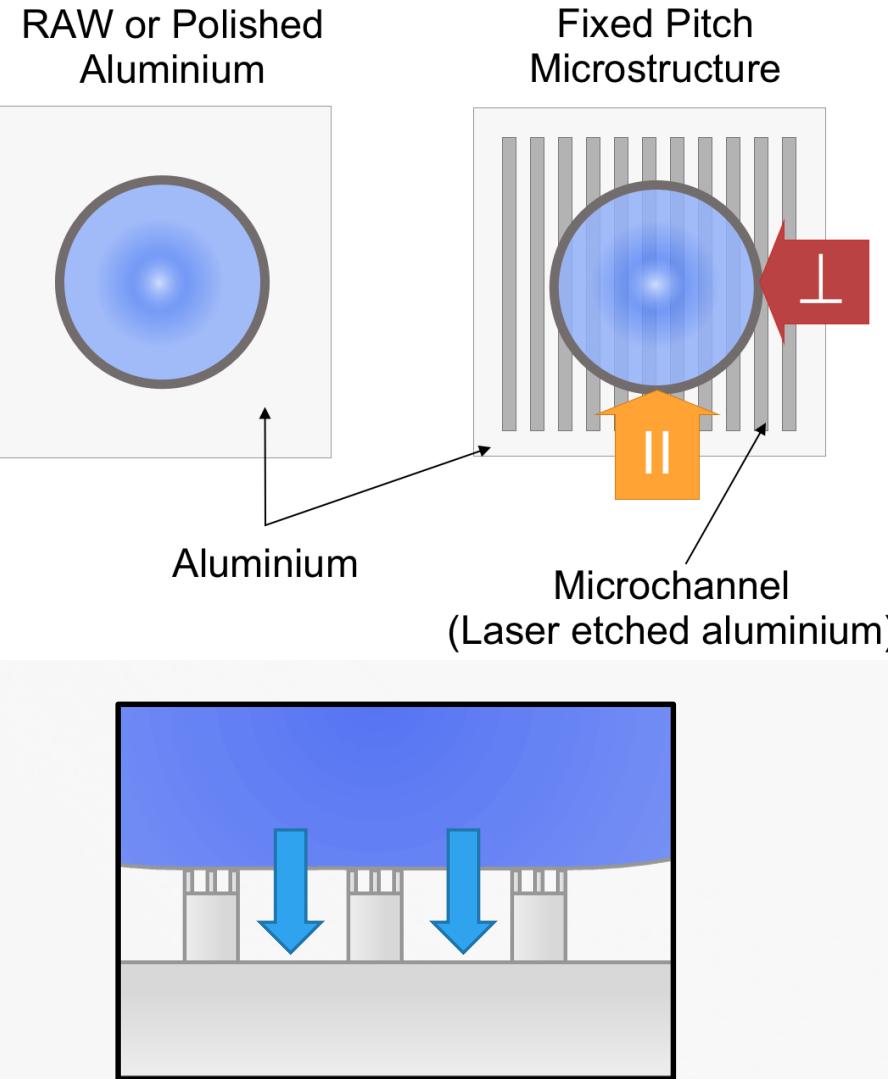


An experiment example
(speed up x5)



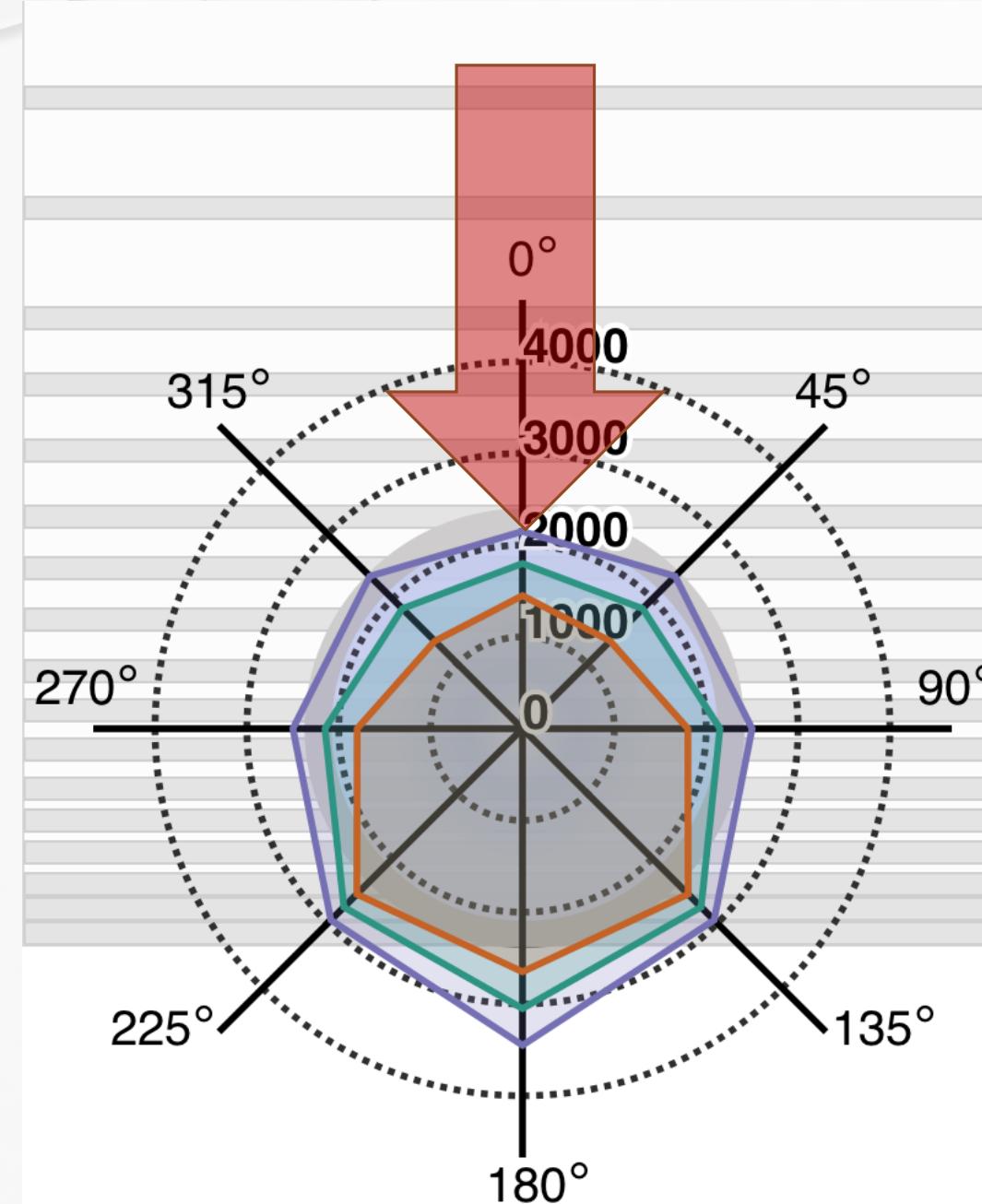
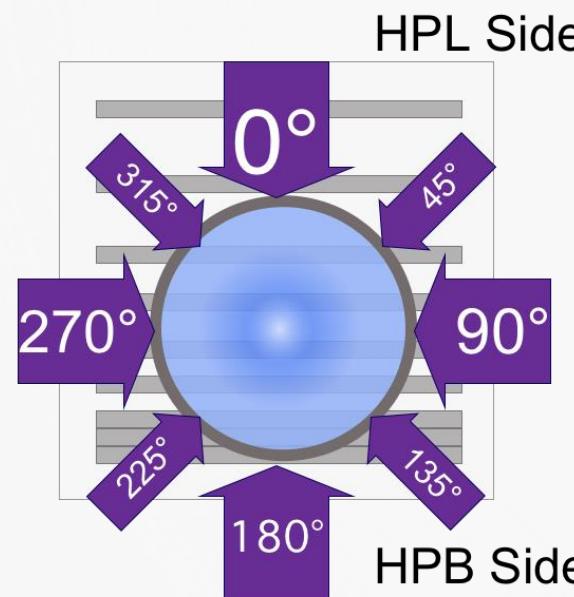
CURRENT STAGE: ICE ADHESION

$$IA_s = F / A_{ice-base}$$



CURRENT STAGE: ICE ADHESION

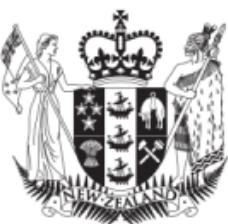
Gradient



Pushing from here requires the same force as polished Al!

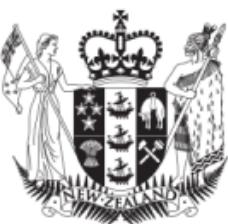
Colour scheme:

- Mean + Absolute Error
- Mean
- Mean - Absolute Error



TOPOGRAPHICAL SURFACE TENSION GRADIENTS FOR EFFECTIVE WATER MANAGEMENT IN ENERGY TECHNOLOGY

- ✓ Gradients provide hydrophobicity;
 - ✓ It is possible to control bouncing-off outcome;
 - ✓ In case of icing, gradients allow to remove ice at a force similar to unprocessed aluminium;
 - ✓ Survived after 100 ice removal cycles;
 - ✓ Applicable for various fields;
- 
- 



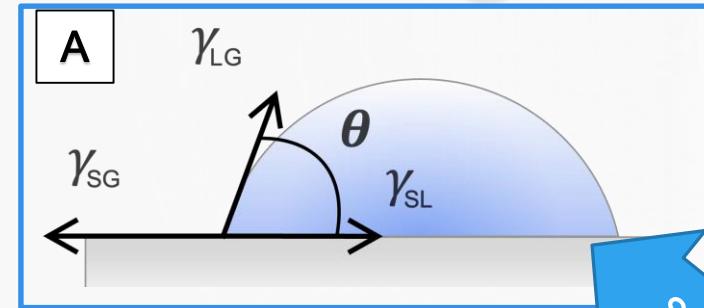
Kirill Misiiuk

Sam Lowrey, Richard Blaikie,
Andrew Sommers, Geoff Willmott

Thank you for your attention!

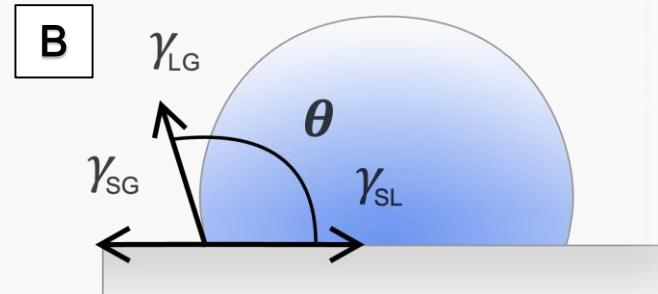
FUNDAMENTALS: STATICS

Solid-liquid interaction



Young's equation

$$\gamma_{SG} = \gamma_{SL} + \gamma_{LG} \cos \theta$$



Contact angle of a flat surface.
 (A) hydrophilic (HPL, $0^\circ < \theta \leq 90^\circ$),
 (B) hydrophobic (HPB, $90^\circ \leq \theta < 180^\circ$),

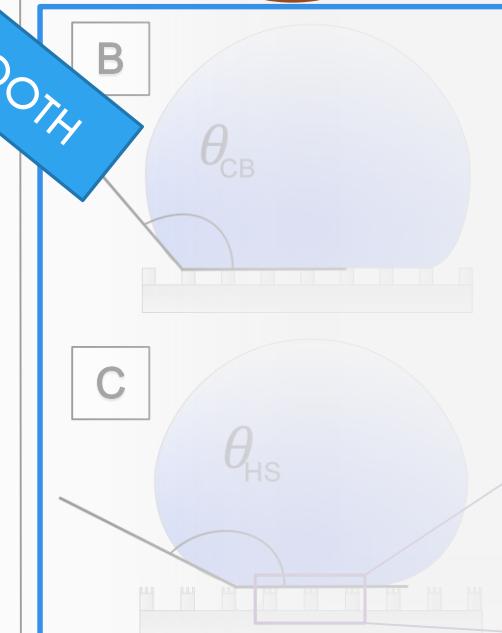
Wetting states



Wenzel equation

$$\cos \theta_W = R \cos \theta$$

R – ratio of the actual surface to the flat projection



Cassie-Baxter equation

$$\cos \theta_{CB} = f_1 \cos \theta - f_2$$

$f_1 + f_2 = 1$, f is the area fraction of an interface (f_1 – solid-liquid, f_2 – liquid-air)

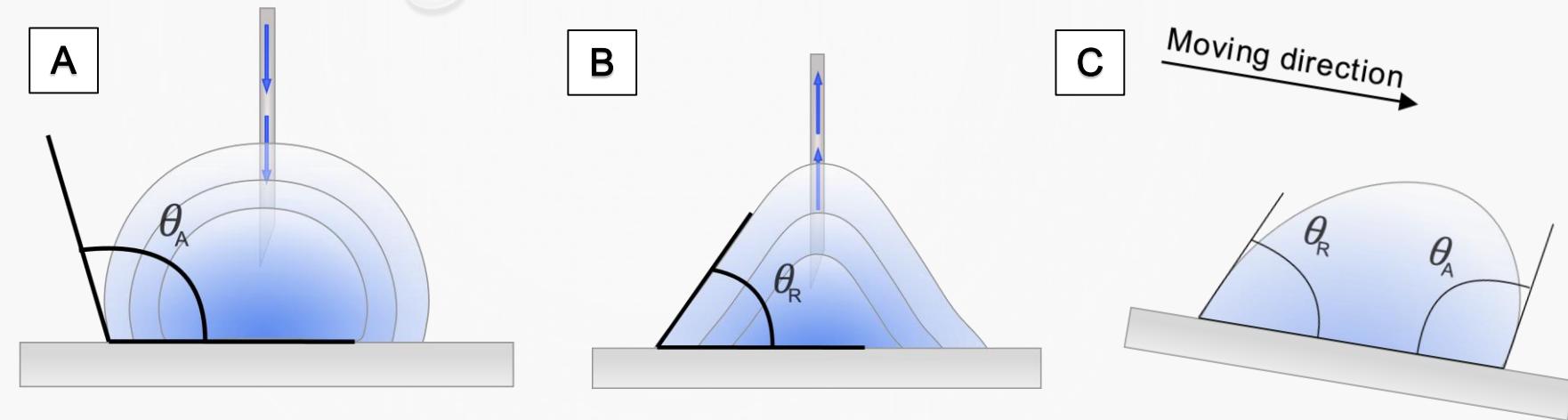


An illustration of the differences of contact models:
 (A) Wenzel's model,
 (B) Cassie-Baxter's model,
 (C) Hierarchical structure with CB-CB states.

FUNDAMENTALS: DYNAMICS

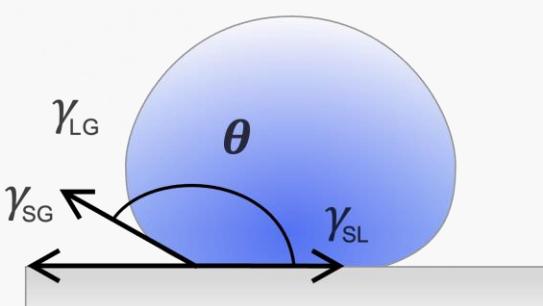
Contact angle hysteresis

$$CAH = \theta_A - \theta_R$$



Schematic of a contact angle hysteresis measurement by
 (A) increasing and (B) decreasing of a droplet volume; (C) “tilting plate”-method, where a droplet is moving over the surface.

$$\theta_R \leq \theta \leq \theta_A$$



Criteria of superhydrophobicity:

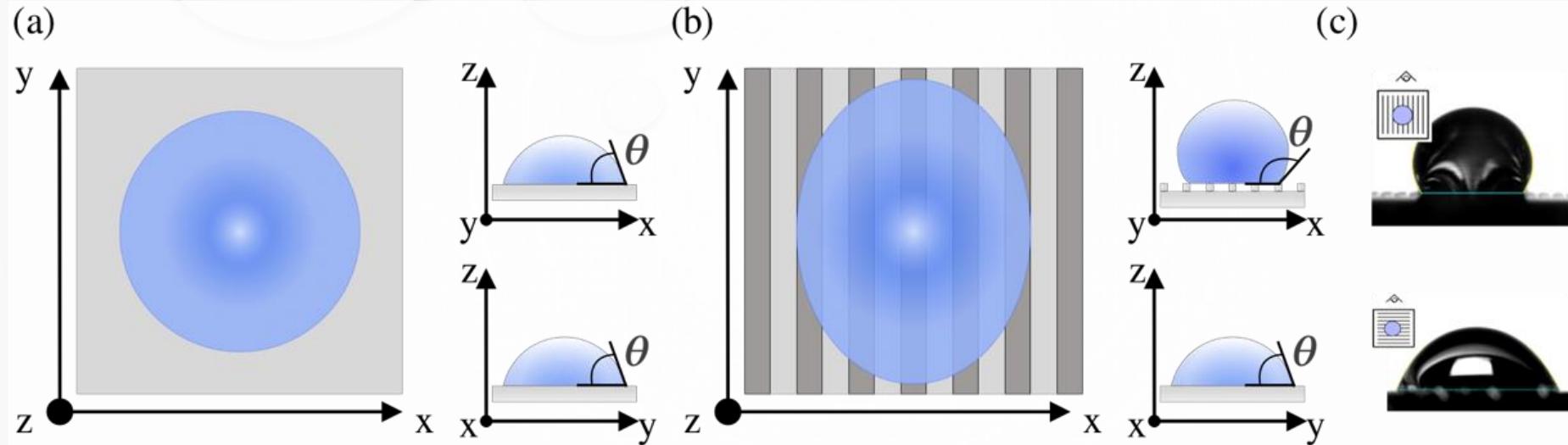
$$CA (\theta) \geq 150^\circ;$$

Less interaction with the surface

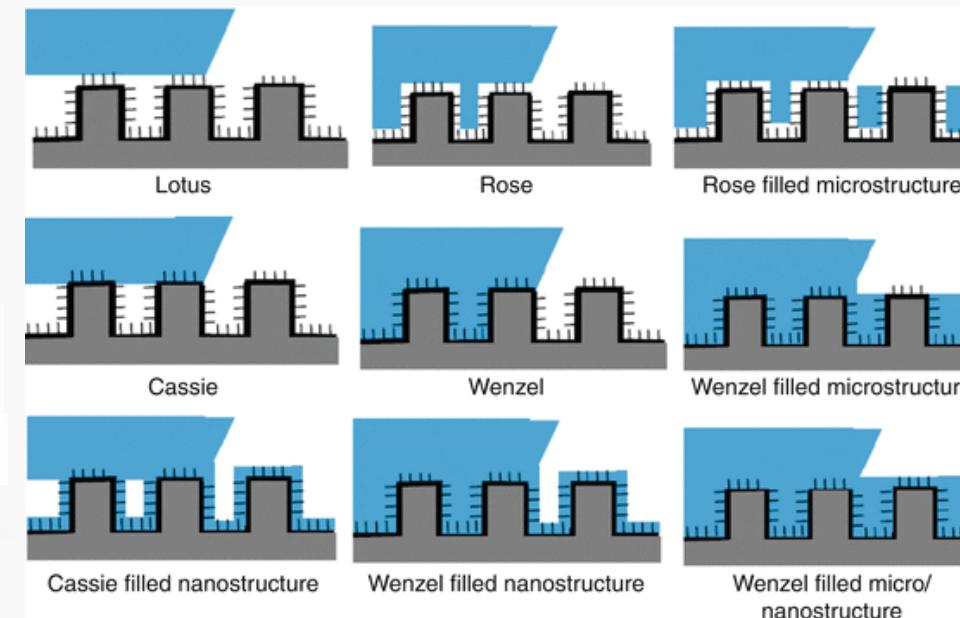
$$CAH \leq 15^\circ$$

Easy to slide/roll off

FUNDAMENTALS: MICRO-WETTING STATE



An illustration of the differences of wetting: (a) isotropic (uniform, randomly rough) surface, (b) anisotropic (grooved) surface, (c) real goniometry photos of anisotropic surface.



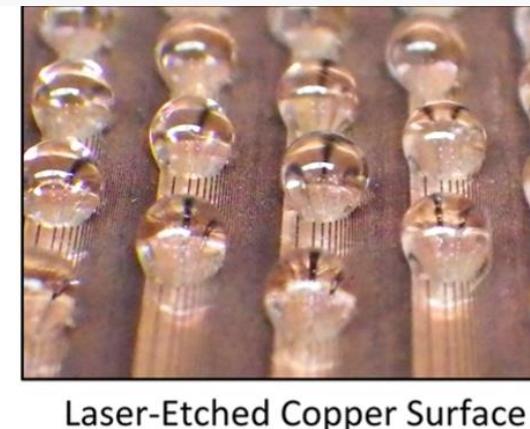
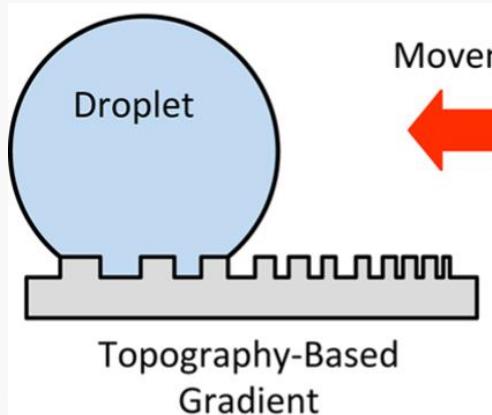
Different wetting states at different scales lead to different droplet behaviour

Bhushan B., Nosonovsky M. (2012) Rose Petal Effect

https://doi.org/10.1007/978-90-481-9751-4_157

TOPOGRAPHY GRADIENT MANUFACTURING IDEAS

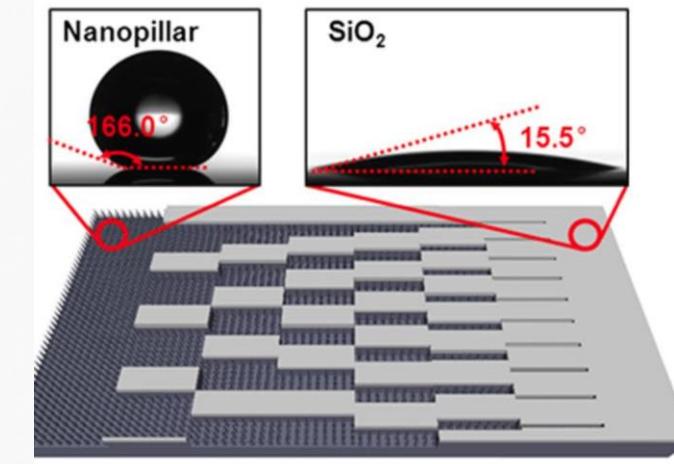
Microgrooves



A. D. Sommers et al., *Langmuir*, 2013, 29, 12043–12050

- made on copper via laser etching;
- Wenzel state (not superhydrophobic);
- relatively short travel distance;

Stripes

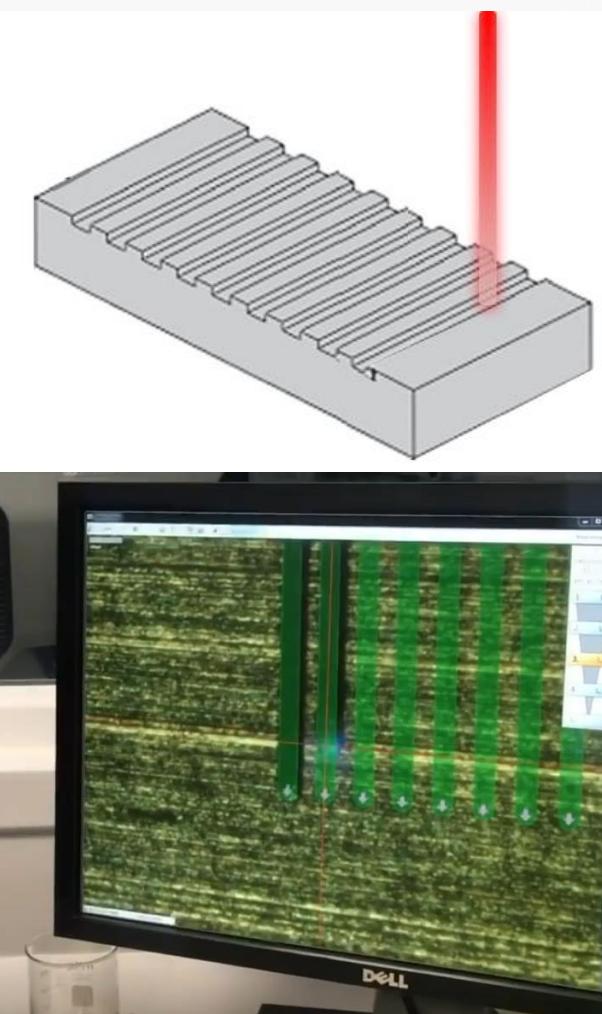


C. Liu et al., *Sci Rep*, 2017, 7, 7552

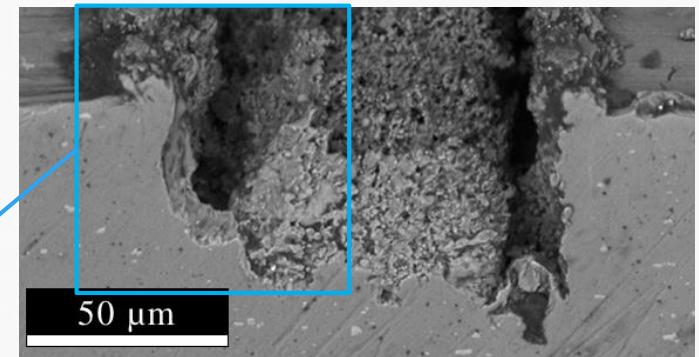
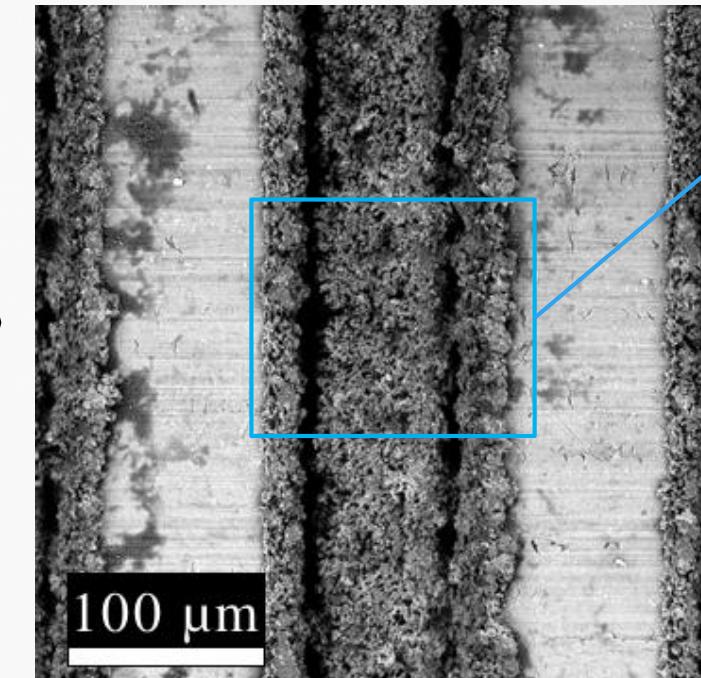
- made on silica/SiO₂ via UV-lithography and reactive-ion etching;
- all wetting states along the gradient;
- relatively long travel distance;

MICROFABRICATION

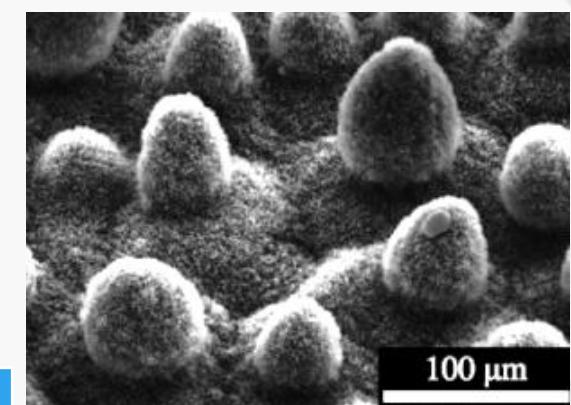
Laser-etching



Resultant structure

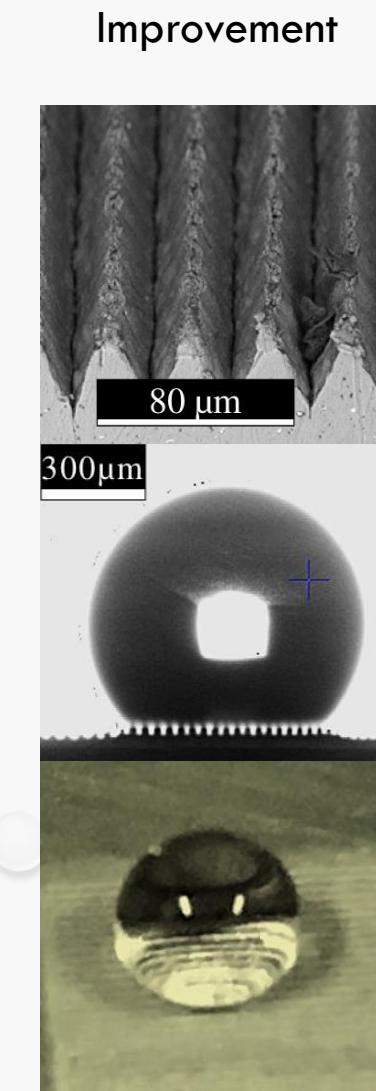
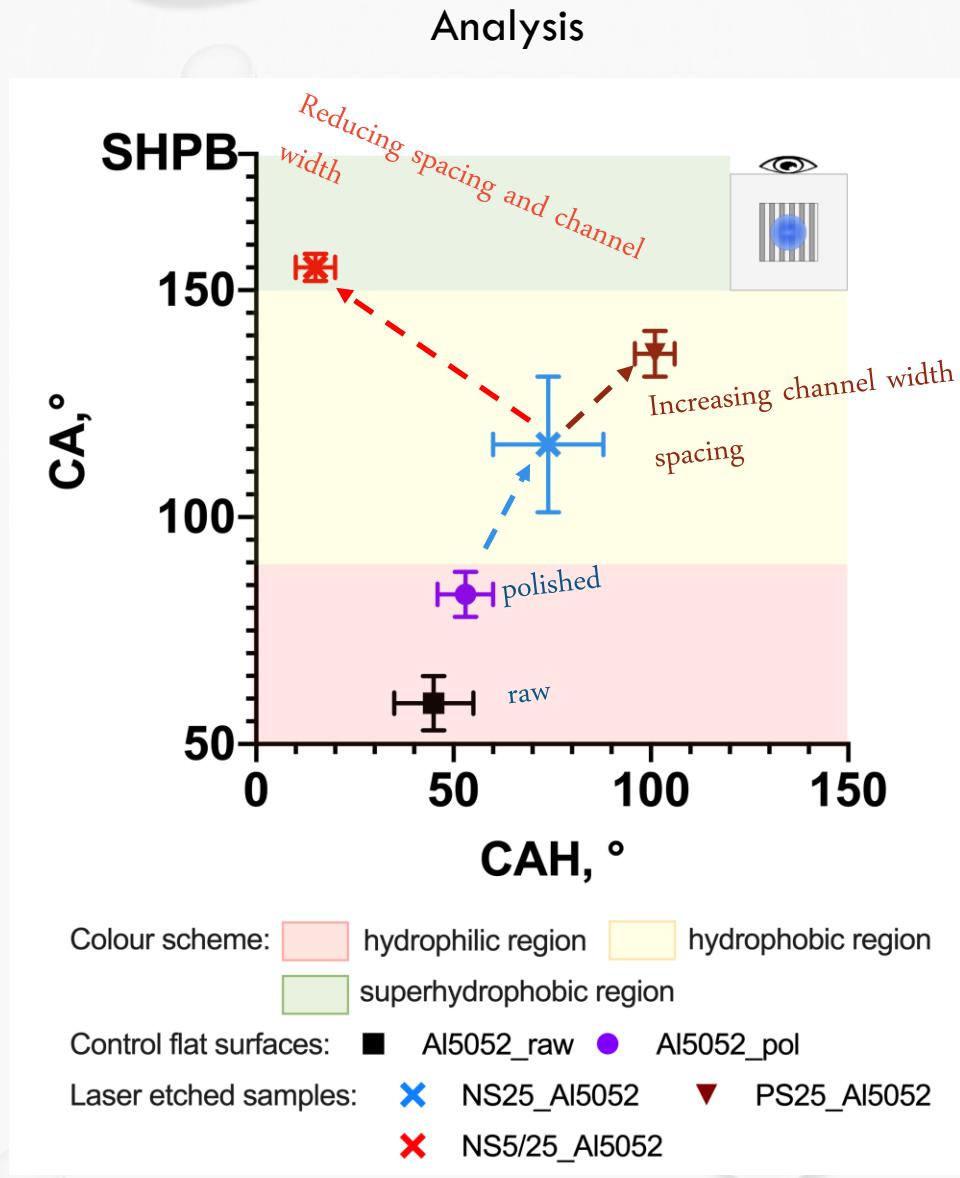
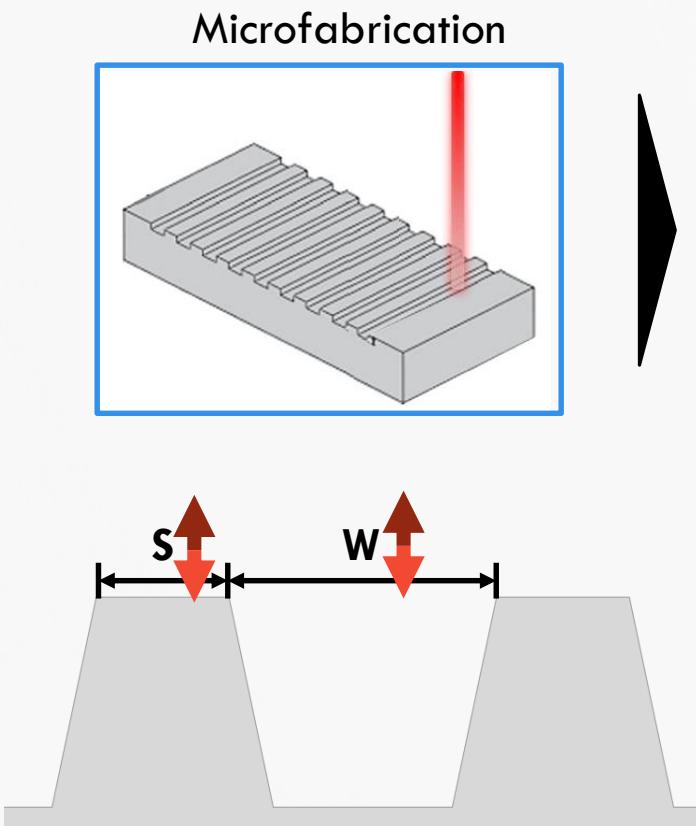


Similar to lotus!

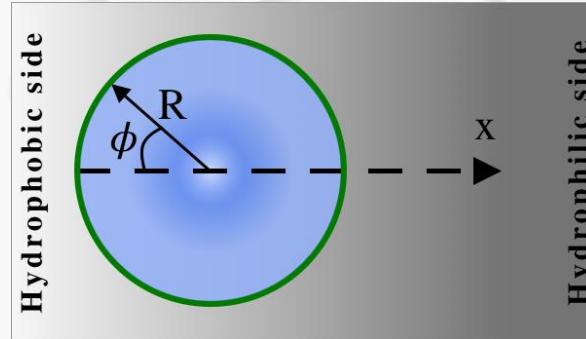


	Microstructure	Nanostructure
Lotus surface	3 – 15 μm	40 – 200 nm
Laser-etching	3 – 20 μm	50 – 250 nm

MICROFABRICATION. WETTING BEHAVIOUR



TOPOGRAPHY GRADIENT MODELLING



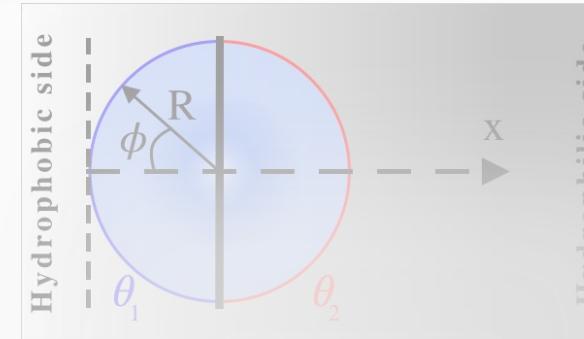
$$F_{acting} = -2\gamma R \int_0^\pi \cos \theta \cos \phi d\phi$$



$$F_{acting} = F_{driving} + F_{hysteresis}$$

$$F_{driving} = \gamma R^2 \pi \frac{d \cos \theta}{dx}$$

$$F_{hysteresis} = 2\gamma R (\cos \theta_R - \cos \theta_A)$$



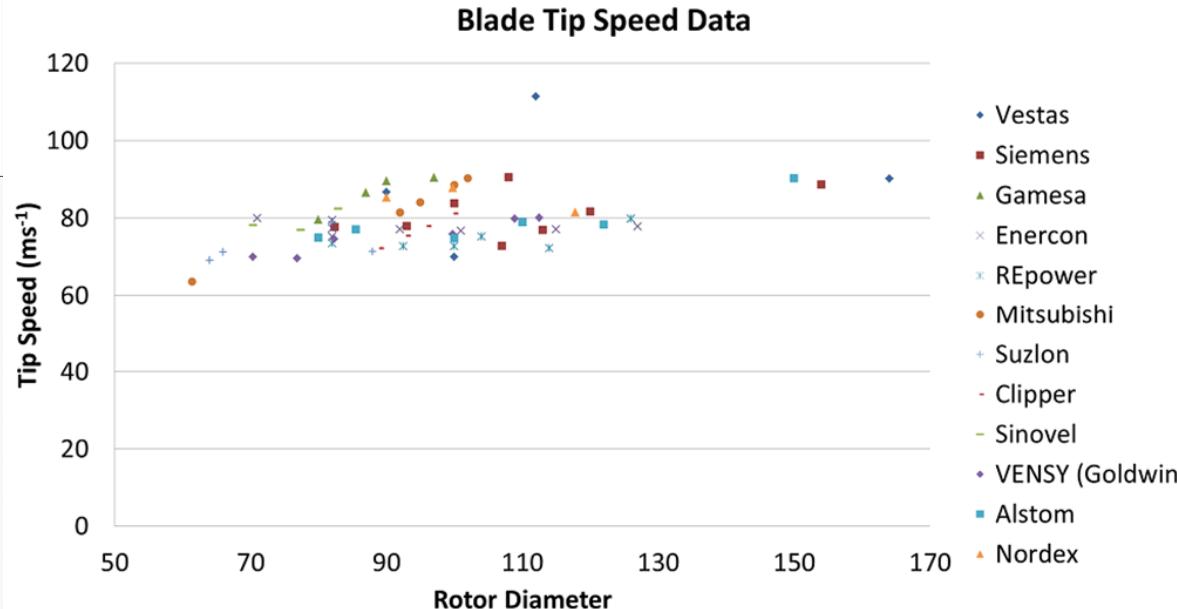
$$\begin{aligned} F_{acting} &= \gamma R \int_0^{\pi/2} [-1 + f(1 + \cos \theta_1)] \cos \phi d\phi \\ &\quad + \gamma R \int_{\pi/2}^{\pi} [-1 + f(1 + \cos \theta_2)] \cos \phi d\phi \end{aligned}$$

where:

$$f = f_0 + \frac{df}{dx} x = f_0 + \frac{df}{dx} R(1 - \cos \phi)$$



DROP IMPACT FROM THE BLADE POV



Blade tip speed versus rotor diameter for various utility scale wind turbine blades [M.H. Keegan et al., J. Phys. D. 46 (2013) 1-20]



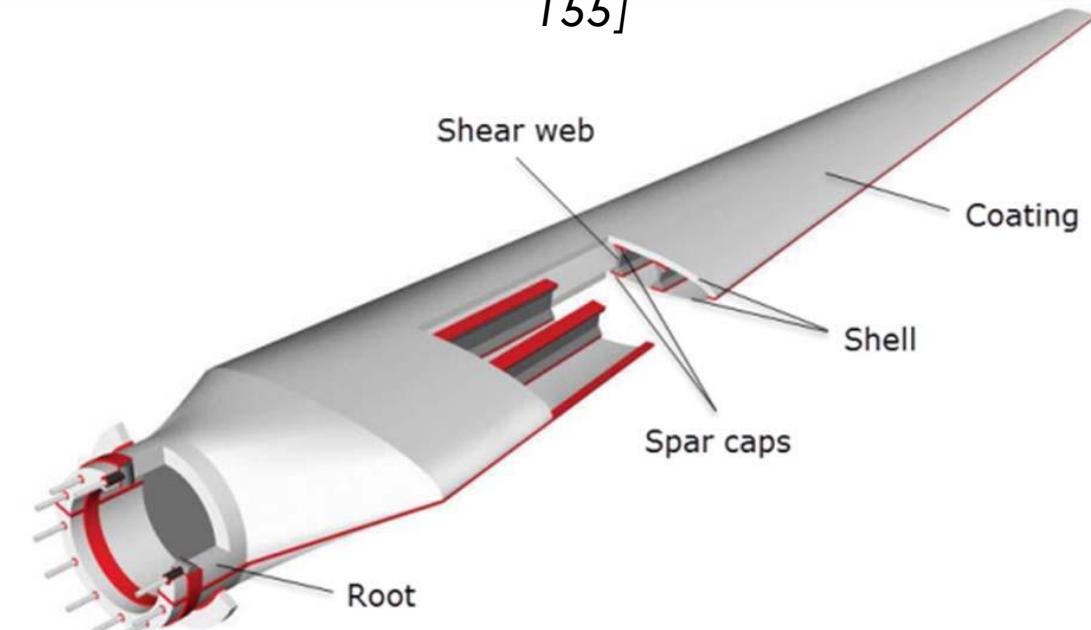
Leading edge erosion of a wind turbine blade

L. Rampel, Wind Systems Magazine (Issue date 24.10.2012) 22-24]

The majority of wind turbine blades use composite materials of thermosetting **polymer** matrix reinforced **with fibers**. The **glass fiber** has been used since the early days of blade manufacturing. **Carbon fibers** are now attracting attention. Other potentially interesting fibers are **aramid**, **polyethylene**, and **cellulose** [P. Brøndsted et al., *Annu. Rev. Mater. Res.* 35 (2005) 505-538].

Wind turbine blade structure.

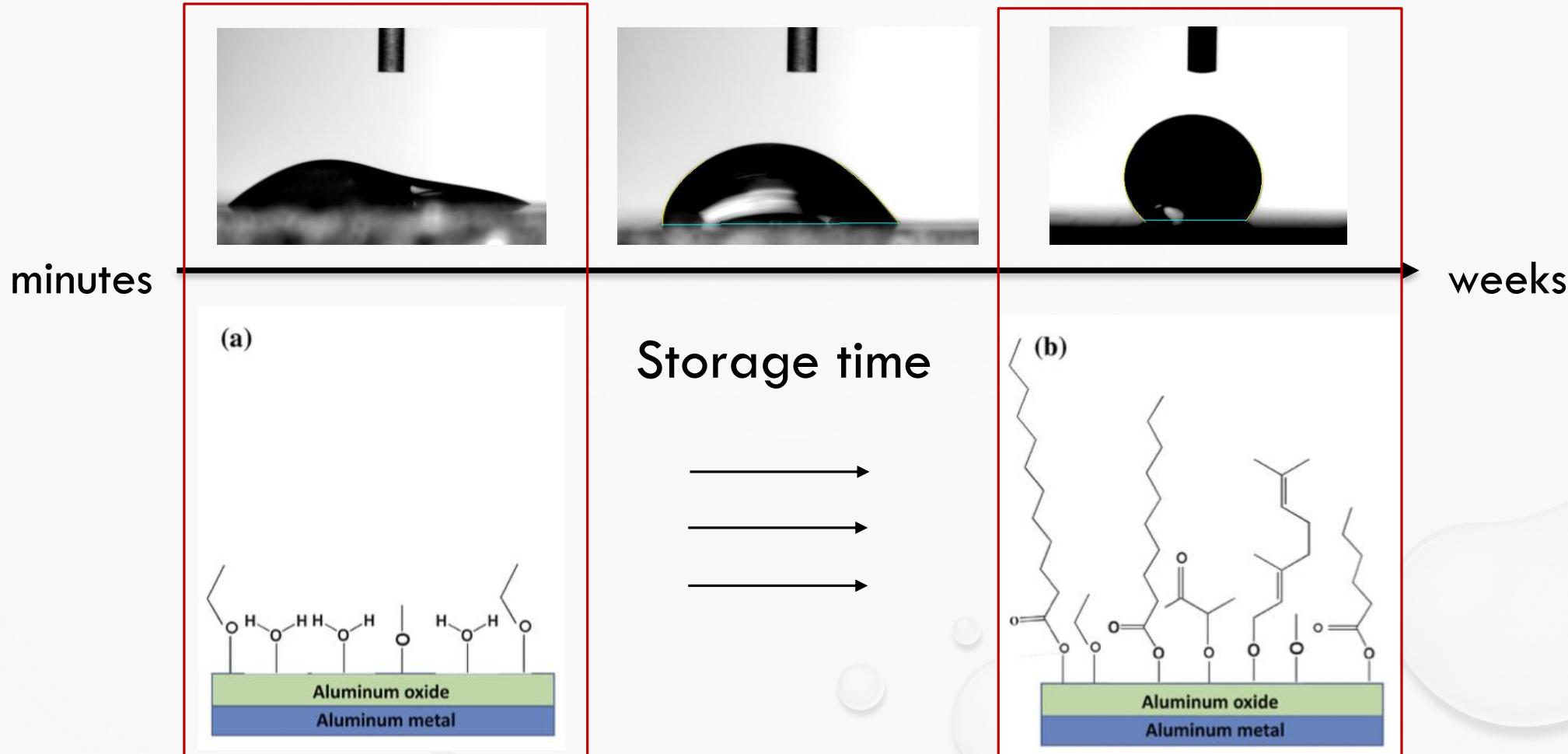
[P. Roth-Johnson et al., *Renewable Energy*. 71 (2014) 133-155]



STRUCTURED ALUMINIUM: ACCOMPANYING EFFECT

Goniometry photos of a 5 μL droplet at the same spot of a laser-etched sample after various storage time

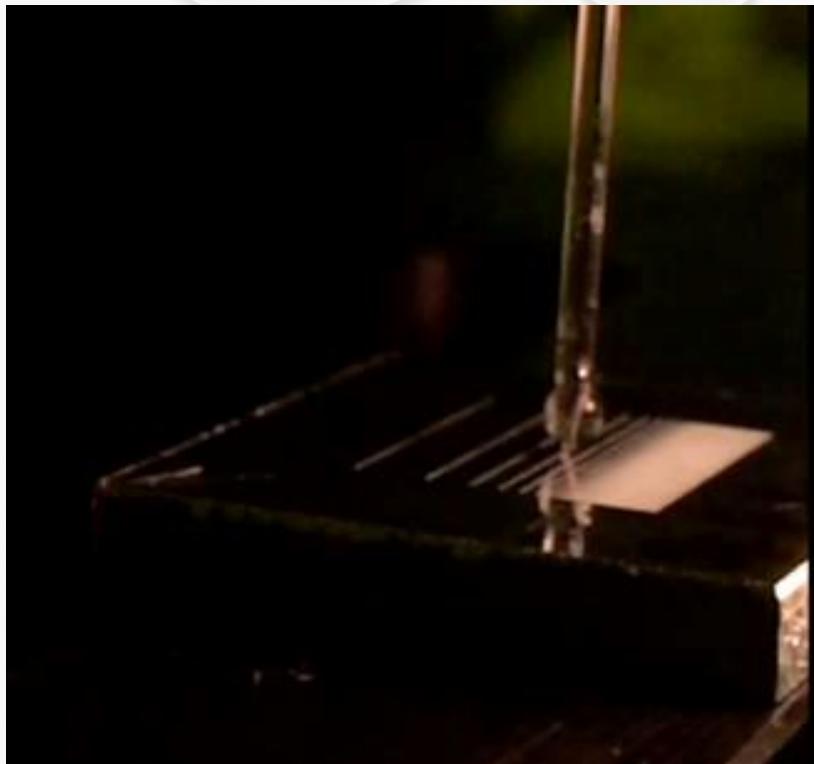
(K. Misiiuk et al., *Langmuir*, 2022, DOI:10.1021/acs.langmuir.1c02518)



[J. Long et al., J. Colloid Interface Sci., 441, 2015]

[G. Schnell et al., Nanomaterials, 10, 2020].

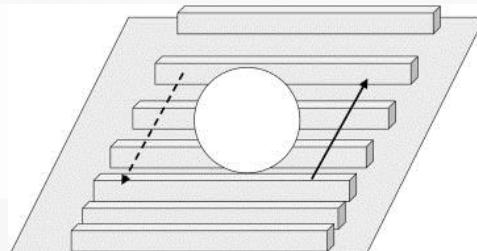
BIDIRECTIONAL MOVING



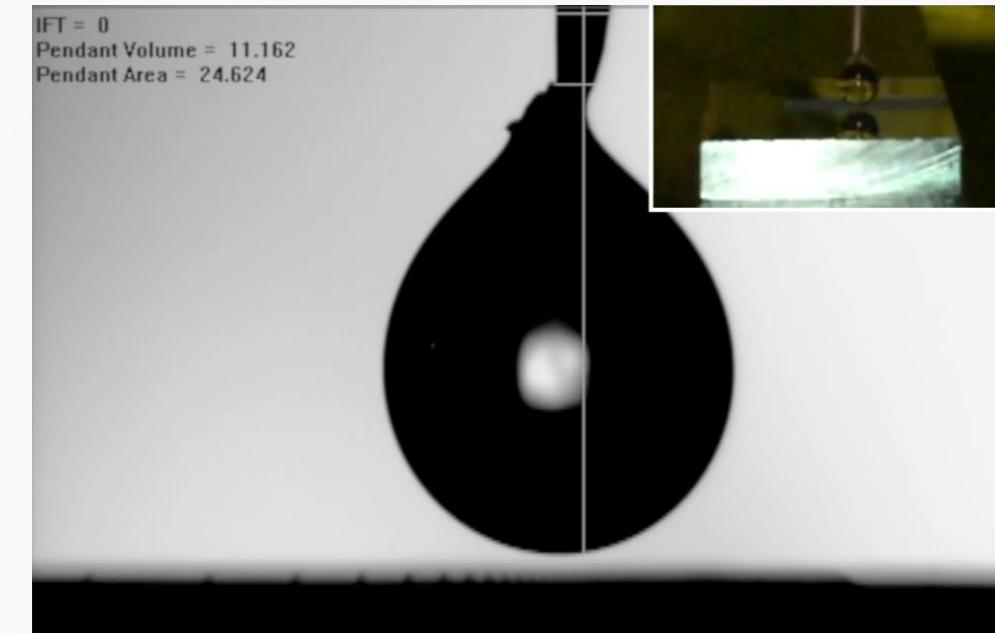
Spontaneous moving (at least directional spreading) in Wenzel state

It's in agreement
with Sun et al.

doi:10.1016/j.tsf.2008.01.011.



(< Fig. 2 from the paper). Schematic illustration of a droplet movement on a roughness gradient surface. The moving behaviour depends on the wetting mode. The droplet moves in the direction pointed by the solid arrow when the wettability is governed by Wenzel theory. If the droplet is in Cassie-Baxter state, it moves in the converse direction indicated by the dashed arrow.



Spontaneous moving in Cassie-Baxter state (the droplet ends up in Wenzel state)